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(54) Title: PAINT COMPOSITION

#### (57) Abstract

Paints and coating compositions, especially those having insulation properties, in particular thermal insulation. The present invention provides for the addition to a hardenable base, of silica, or bagasse or a combination of both, as well as a method of production of the coating composition. Preferably, the hardenable base will form a high build coating when dried or hardened.

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#### PAINT COMPOSITION

The present invention relates to coatings and paints and in particular, insulating coatings and paints which provide heat insulation.

The paint industry has been, for many years trying to develop a thermo-insulating paint which can satisfactorily prevent heat loss or heat gain across painted surfaces.

This is evidenced by West German application 311,7484 which dealt with the addition of sodium bicarbonate and steric acid to paint; Japanese application 4P57102967 by the addition of Potassium titanate fibres and glass frit; Japanese applications 4P58167657 and 4P83164657 by the addition of aluminium flakes, glass wool and polo filler; USSR application 1014812 by the addition of perlite and mineral wool; USSR application No. 286198 by the addition of glass wool and calcium cyanate; and finally USSR 481584 by the addition of perlite and boric acid.

Each of these is of somewhat limited value. The major problem which is faced by paint manufacturers and in particular those trying to develop an effective insulating paint, is being able to add sufficient insulating raw materials and at the same time maintain a thin paint film.

This problem causes increased costs due to thickness of film, as well as extra weight being carried by the coated objects. Further difficulties arise in applying the paint to the articles to be coated.

DEFINITIONS

Throughout the specification and claims, the term "liquid" will be understood to include amorphous, gelatinous, fluid and pourable substances. Further, throughout the specification, the appearance of an asterisk (\*) denotes that the substance mentioned is identified by its Trade Mark or registered Trade Mark.

In the art, the subject of this application, a high build coating is considered to be a coating, which when dried would be of a thickness in the range of 100 microns

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(approx.) up to 5 mm (approx).

It is an object of the present invention to provide a thermal insulating coating, and a method of producing same.

- According to another aspect of the present invention there is disclosed an insulating coating composition comprising:
  - (a) a hardenable liquid base; and
  - (b) either silica or bagasse
- 10 According to a further aspect of the present invention there is disclosed an insulating coating comprising:
  - (a) a hardenable liquid base;
  - (b) silica; and
- 15 (c) bagasse.

According to another aspect of the present invention there is disclosed a method of producing an insulating coating, said method including the steps of:

- (a) collecting bagasse;
- 20 (b) grinding and/or particulating said bagasse to an average particle size of 0.01 mm to 5 mm; and
  - (c) mixing the now particulated bagasse into a paint, coating or like substance.

Bagasse is a natural substance and is the term

applied to the final crushed fibre remaining after

milling of sugar cane. It consists of fibre

(cellulose), water and a small quantity of sugar. It is

generally used as or made into fuel, feed, and fibre

board.

Bagasse is the main source of fuel in the production of steam for mill operation. In some countries, bagasse is a raw material used for the manufacture of paper.

According to a preferred aspect of the present invention there is disclosed an insulating paint, said paint comprising a paint base which produces when dried, a membrane of a substantially high build coating; and up to 60% by weight of a combination of silica and bagasse.

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preferably the silica used is a granular type having a hollow centre, whilst the bagasse is preferably dried then ground up to a consistency wherein the average size of particles is approximately 0.01 mm to 5 mm.

Good results have been obtained with a silica known as Q-CEL 450\* silica microspheres, which is combined with bagasse into a high build membrane paint.

Q-CEL 450\* or Q-CEL 500\* are hollow organo silicon modified borosilicate microspheres and as a commercial product are sold as an odorless dry white powder. The microspheres are readily wetted out by organic fluids but resist wetting by water. They typically have a bulk density of 0.105 gm/cm<sup>3</sup>; a typical effective density/liquid displacement of 0.15 to 0.5 gm/cm<sup>3</sup> with a mean particle size (diameter) of 65 to 70 microns ranging between 10 to 200 microns.

Other forms of silica can be utilised, such as hollow organo silicon modified borosilicate microspheres of different dimensions, solid glass microspheres, which are manufactured from A-glass, which are commercially available in graded sizes from 5 to 5000 microns; ceramic, polymeric and mineral microsperes. Further, combinations of these different "silicas" can be utilised.

The natural substance bagasse can be replaced by an artifically manufactured substance whose chemical composition is any one of the following, or a combination of any one of the following:

- A) Dry cellulose: approx 40% by weight
  Pentosan: approx 22% by weight
  Lignin 19% by weight
  Ash: approx 20% by weight
  Impurities (incl: water, raw sugar and dirt) approx
  17% by weight
- B) Holo cellulose: approx 60% by weight; and
- 35 C) Moisture content: approx 49%

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Insoluble solids: approx 48.7% Soluble solids: approx 2.3%

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Each of A, B and C a the chemical breakdown of bagasse and percentages mentioned can be varied to produce differing properties. In the case of natural bagasse, the chemical breakdown and properties may alter depending upon methods used to grow the sugar cane and the climate and location where the sugar cane is farmed.

The hardenable liquid base can be a paint or paint base such as an acrylic membrane paint, a copolymer resin, an alkyd resin and any other suitable coating, or liquid base, which will harden.

Examples of the present invention will now be described with reference to experimental results and the figures of the drawings in which:

Fig. I illustrates a test rig;

Fig. 2 is a graphical representation of the results of tests conducted over a 6 hour period on a dried film of a paint to the present invention; and

Fig. 3 is a graphical representation of the results of tests conducted over a 48 hour period on the same film of that whose results are shown in Fig. 2.

#### INSULATING PAINT EXAMPLE 1

A sample of insulating paint was produced from a paint base, this paint being of an acrylic membrane type as is commonly known in the industry. To this paint base was added 10% by weight of specially treated bagasse. This special treatment consisted of a ground down or particulate bagasse of approximately 0.01 mm to 0.5 mm.

To this was further added 5% by weight of Q-CEL 450\* spherical silica.

These were mixed by means of gentle paddle stirring.

The paint mixture was then applied by roller to produce:

- 35 (a) a membrane of dried paint; and
  - (b) a piece of galvanised sheet metal coated with the paint.

#### TESTING

A heat harrier membrane test was devised to measure 2/11/05, EAST Version: 2.0.1.4

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the insertion loss of membrane, at average and normal temperature, in conditions simulating actual use on roofs, and situations generally where ambient temperatures exists on reverse surface of membranes and a higher temperature exists on the obverse surface.

## TEST APPARATUS - (See Fig. 1)

The apparatus consisted of 2 cylindrical chambers 1 and 2 fabricated from galvanised sheet steel of 1 mm thickness.

10 Each chamber 1 and 2 has two concentric cylinders 3 and 4 of height 60 cm. Inner cylinder 3 has a 30 cm diameter and outer cylinder 4 has a 40 cm diameter with space 5 between filled with insulation 6 and end spaces sealed with galvanised sheet.

Chambers 1 and 2 have galvanised sheet flanges 7 at each end, being some 60 cm square with 30 cm hole 8 in centre and 3 heat sensitive probes 9 sited 120° apart, round the periphery, spaced 5 cm from one end.

Chambers 1 and 2 are stacked vertically. Lower chamber 2 is heated as required and upper chamber 1 is at ambient temperature of laboratory area, being open at the top.

The design of chambers 1 and 2 and their volume is an optimum compromise between 2 conflicting factors:

- 25 1. It should be large enough to permit valid testing
  (a sample of membrane say 600-1000 square cm, is a
  reasonable size) and avoid the difficulties
  inherent in arranging a very small heat supply with
  adequate control; and
- 2. It should be small enough not to require excessive heat input, with the control and insulation problems inherent in containing large amounts of heat, and particularly, circulating air currents minimized so that the temperature measured on both
- membrane (15) surfaces is sensibly the temperature over the total area.

A unit assembly of radiator 10 with infrared lamp 11 and incandescent lamp 12 as the heat source in the bottom of lower chamber 2 and having an electric current 2/11/05, EAST Version: 2.0.1.4

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supply at 50 hertz, variable in steps of 1 volt, which is read on a meter connected across the unit input.

Voltage variation is by WF8(G.R.) Variac\* rated at 10 amps, with 60 volts connected across its 0-280V winding, so providing an effective 'band-spread' of more than 4 times that of the Variac scale.

During programming of apparatus, the voltage was calibrated against temperature (after it had stablised) and a scale compiled, so in running the test series, repeat results were reliable and predictable. Tests were repeated 10 times.

The 3 Type G probes sited 120° apart in top end of bottom chamber 2 and bottom end of top chamber, were connected to a Zeatron GPE\* remote reading electronic thermometer and thus 3 readings were obtained in each chamber 1 and 2.

Probes 9 were 5 cm from flange 7 in each chamber 1 and 2 because:

- 1. Heat rose in bottom chamber 2 so the temperature
  20 was measured 5 cm down from the top was sensibly
  that over the membrane lower surface 15b, circa
  40 cm from heat source, thus simulating commercial
  and domestic application of membrane 15 in actual
  use; and
- 25 2. Top chamber 1 at ambient temperature has probes 5 cm from membrane upper surface 15a so any heat passing membrane will rise and probes will indicate this.

#### ME THO D

In this test rig the lower surface 15b is the obverse surface whilst the upper surface 15a is the reverse surface. To some extent these test conditions were harsher than actual use conditions as the obverse surface is usually upwardly facing and thereby allows for more cooling and transfer of heat by convection.

Sample membrane 15 was clamped between flanged ends 7 of the chambers 1 and 2 and through bolted to prevent air leakage.

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Heat was supplied to bottom chamber 1 and temperature recorded as the average between 3 probes, which differed slightly due to unavoidable air current. Chamber 2 therefore proved, close to ideal. Probes in top chamber 1 showed no variation, as predicted.

#### RESULTS

The insulating paint of example 1 is a heat barrier, providing almost 99% insertion loss when tested under conditions simulating actual use on roofs and similar use.

No variation of any significance was observed between:

- 1. Membrane alone; and
- 2. Membrane on galvanised sheet.

The measurements recorded in these tests for membrane 15 alone are graphically represented in Figs. 2 and 3.

In Fig. 2 the lefthand margin represents degrees celcius whilst the the bottom margin represents hours from the start of the test. The upper graph represents the temperature of the membrane whilst the lower graph represents the ambient temperature.

The heat source remained stable at  $40^{\circ}$ C, one hour after the start of the test run. The 3 probes read to within  $1^{\circ}$ C of each other.

In Fig. 3 the lefthand margin represents degrees Celcius whilst the bottom margin represents the time of day with ambient temperature being varied according to natural conditions over a 48 hour period. The figures at the bottom margin represent the time on a 24 hour clock.

The upper graph represents the temperature of the membrane whilst the lower graph represents ambient temperature.

The tested membrane had one smooth and one rough surface. As the membrane tested was not of continuous cross-section, (in fact varying from approx 0.2 mm to approx 0.6 mm in some places), this exaggerated the reading for the heat gain of the membrane.

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## THERMALLY INSULATING COMPARATIVE EXAMPLE (CONTROL)

The tests conducted or membrane and membrane on galvanised sheet were compared to a "Batt", which is a type of fibreglass insulation used generally by the building industry to insulate roofs and other building elements.

The batt tested was a rated R2.5 (see Standards Association of Australia A.S. 2627 Part 1, 1983).

when tested under the same conditions as the membrane and membrane on galvanised sheet, the performance of the batt was not significantly different from that of the membranes.

## (CONTROL) NON INSULATING PAINT EXAMPLE

The paint base used to manufacture the insulating paint of example 1 was taken separately and a film of same was produced. This film was placed in the test apparatus and the obverse surface was subjected to a temperature of 40°C. The initial temperature measurement on the reverse side was measured at 32.3°C at an ambient temperature of 21.1°C and was measured one hour after the 40°C temperature had stabilised in the heat source chamber.

Subsequent measurements recorded an increase in the reverse side temperatures such that with the effluxion of time, both sides were within  $2^{\circ}$ C of each other. That is the obverse was  $40^{\circ}$ C whilst the reverse side was  $38^{\circ}$ C.

## SHEET METAL COMPARATIVE EXAMPLE

A piece of sheet metal, such as that coated with the insulating paint of example 1, was tested in an uncoated condition.

The galvanised sheet metal was placed in the test apparatus and the obverse side was subjected to a temperature of  $40^{\circ}$ C. The initial temperature measurement on the reverse side was measured at  $30.6^{\circ}$ C at an ambient temperature of  $21.1^{\circ}$ C, and was measured one hour after

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the 40°C temperature had stabilised in the heat source chamber.

Subsequent measurements recorded an increase in the reverse side temperature, such that with the effluxion of time, both sides were within  $2^{\circ}$ C of each other. That is the obverse side was  $40^{\circ}$ C whilst the reverse side was  $38^{\circ}$ C.

Further test have been conducted in open air conditions at experimental test sites in Australia.

#### ALLUNGA TEST RESULTS

Tests were conducted in far north Queensland,
Australia at Allunga, (Lat 19 15'S Long 146 46'E) where
temperatures were measured between 11.45 a.m. and 12.45
p.m. in degrees Celcius, on days of little or no cloud.
The galvanised steel sheds (two were constructed) were
identical and erected in parallel position approximately
3 metres apart. Temperature probes were fixed in
identical positions in each shed at a position 1 cm below
the centre, inside, and doors were closed at all times.

20 Results were as follows:

		· · · · · · · · · · · · · · · · · · ·	
	Date	Paint Insulated	Unprotected Shed
		Shed OC	oC
25	October 28	39	44
<b>4</b> .5	29	37	40
	30	38 <sup>.</sup>	45
	31	36	41
	November		
30	8	38	42
	11	40	49
	13	37	43
	15	39	46
	18	41	49
35	25	40	51
	28	43	53
	December		-
	2	40	48
	4	39	45
40	4 8 9	43	42
	9	42	50
	10	43	50

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		Date	Paint	Insulated
		Unprotected Shed		
		Shed		oC
5	December - Cont.	40		47
	12	40		**
	14	43		50

On the days of December 8th, 9th, 10th, 12th and 14th, the outside temperatue in the sun was recorded as being  $33^{\circ}$ ,  $34^{\circ}$ ,  $35^{\circ}$ ,  $34^{\circ}$  and  $33^{\circ}$  C respectively.

## SYDNEY TEST RESULTS

Further tests were run in Sydney, Australia (Lat 33° 55'S, Long 151°10'E) over a 3 month period. When building the shed, foundations were laid using ordinary kiln fired building bricks, and a platform laid on said foundations. Both sheds were exposed to the same temperatures in each 24 hour perod.

The results were as follows:

Maximum Temperatures

20	-		Recor	<u>ded</u>
	Date		Paint Insulated	
		Conditions	Shed	Shed
		-	OC	oc
	<b>~</b> 1 1			
	September		. 20	26
25	5 7 9	Clear, S.W. winds	20	26
	7	Clear, W. winds	18	26
		Cloudy, W. winds	23	29
	11	Calm, cloudy	21	27
	13	Calm, Cloudy	21	28
30	15	Calm, sun	22 ·	29
•	· 17	Calm, cloudy	21	28
	19	Calm, cloudy, rain	20	25
	21	Sun, fine, calm	18	25
	23	Sun, fine, calm	24	29
35	25	Cloud	26	32
<b>J</b> J	27	S. winds	19	25
	29	Calm, cloud	22	29
	29	Caim, Cloud	22	43
	October			•
	1	Calm, clear, sun	25	32
40	3	Calm, sun	26	32
- •	3 5 7	Wind - change to so	outh 28	35
	7	S.S.W. winds, cloud		29
	ý 9	Calm, cloud, shower		30
	11	Clear, change to S.		34
	4.4	p.m.	WINGS 27	
45	13	reme	17	17
40	2	/11/05, EAST Version	: 2.0.1.4 <del>-</del> '	

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## Maximum Temperatures

## Recorded

	Date		Insulated	Unprotected
	<del></del>	Conditions	Shed	Shed
5	•		OC	oC
	October -			
	15	Light S. winds, cloud,	21	26
		clearing		
	17	Sun, clearing	23	29
10	19	Rain a.m.; cloud	21	25
	21	Clear, sun, calm	22	28
	23	Cloud, showers, clearing	26	31
	28	Clear, sun	22	27
	29	Clear, sun	20	26
15	31	Clear, sun	23	29
				•
	November		- 4	20
		Clear, sun, N.E. winds	24	30
	3 5 7	Clear, sun, N.E. winds	27	33
	5	Cloud	28	35
20		Cloud, sun, calm, humid	27	34
	9	Clear, sun, calm	28	34
	11	Cloud, S.E. winds, shower		32
	13	Cloud, N.W. winds - sligh		29
	15	Cloud, S.W. winds, rain	26	32
25	17	Cloud, S.E. winds, shower		33
	19	Clear, calm	21	28
	21	Cloud, S.E. winds - fresh		28
	23	Cloud, S.E. winds, fresh	25	31
	25	Cloud, S.E. winds - sligh		30
30	27	Cloud, S.E. winds, shower		33
	29	Cloud, S.E. winds, shower	s 24	30
	_			
	December		04	3.1
	1	Cloud, S.E. winds, shower		31
	3	Calm, rain	24	29
35	5	Calm, light cloud	26	33

## FURTHER INSULATING PAINT EXAMPLES

### Example 2: STYRENE ACRYLIC HARDENABLE BASE.

#### HARDENABLE BASE:

	BASF 290D Acrylic*	322	Kgs
5	Dispex N40*	3.4	Kgs
-	Beveloid 60*	2.3	Kgs
	Corflex 880*	4.6	Kgs
	Basf S.300 Acrylic*	32.0	Kgs
	Titanium Dioxide	60.0	Kgs
10	Calcium Carbonate	100.0	Kgs
	Water	52.0	Litres
	M.D. 13 (Mercury)*	1.75	Kgs
	Corsal EEA*	7.5	Kgs
	White Spirits	11.5	Litres
15	Ammonia	2.75	Litres

BAGASSE: 90 Kgs.

This amount represents approx 12.5% by weight

of the total composition.

SILICA: Hollow organo silicon modified borosilicate

microspheres: 30 Kgs. This amount represents

approx 4.2% by weight of the total composition.

## Example 3: ACRYLIC HARDENABLE BASE

#### HARDENABLE BASE:

	Ethylene Glycol	7.41	Kgs
25	Water	42.0	Kgs
	Natrasol 250 HR*	.86	Kgs
•	Orotan 731 25%*	2.39	Kgs
	Triton G.F.10*	.20	Kgs
	M.D. 13 (Mercury)*	•5	Kgs
30	Texanol*	4.4	Kgs
	Titanium Dioxide	15.0	Kgs
	Calcium Carbonate	40.0	Kgs
	Talc	17.0	Kgs
	Silica 140 Mesh	17.35	Kgs
35	Primal AC 388*	115.0	Kgs
	Silica 140 Mesh	8.67	Kgs
	Beveloid 60*	.400	Kgs
	E.T.P	3.0	Kgs
		To Vis	scosity

40 BAGASSE: 42.0 Kgs. This amount represents approx 12.7% by weight of total composition excluding water added for viscosity.

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SILICA: Hollow organo silicon modified borosilicate:
14.0 Kgs. This amount represents approx 4.2%
be weight of total composition excluding water
added for viscosity.

#### 5 Example 4: ALKYD RESIN BASE

### HARDENABLE BASE:

	White Spirits	46	Kgs
	Alkyd Resin Ml7	92	Kgs
	Alkyd Resin M57	92	Kgs
10	Cereclor 48*	1	Kgs
	Polybutane 100*	6	Kgs
	Titanium Dioxide	40	Kgs
	Zinc Oxide	4	Kgs
	Mica	25	Kgs
15	Calcium Carbonate	50	Kgs
	M.D. 13 (Mercury)*	0.3	Kgs
	Crodaclay*	4	Kgs
	D.A.A.	1	Litre

BAGASSE: 36 Kgs. This amount represents approx 8.8% by

20 weight of the total composition.

SILICA: Hollow organo silicon modified borosilicate

microspheres: 12 Kgs. This amount represents approx 2.9% by weight of the total composition.

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Example 5: COPOLYMER HARDEMABLE BASE COMPRISED OF PLIOLITE RESIN

#### HARDENABLE BASE:

5	Calcium Carbonate Course	20.7 8.5 17.1 7.0 6.5	Kgs Kgs
	Wetting Agent	0.115	Kgs
10	Pliolite AC 80*	6.44	Kgs
_	Pliolite AC 4*	1.61	Kgs
	Chlorinated Paraffin 65	6.67	Kgs
	Mineral Spirits	27.6	Kgs
	Polar Solvent	3.795	Kgs

15 BAGASSE: 15 Kgs. This amount represents 11.8% by weight of the total composition.

SILICA: Hollow organo silicon modified borosilicate microspheres: 6 Kgs. This amount represents 4.7% by weight of the total composition.

20 Example 6: COPOLYMER HARDENABLE BASE

#### HARDENABLE BASE:

	Titanium Dioxide	10.0	Kgs
	Calcium Carbonate	9.5	Kgs
	Course Extender l	9.5	Kgs
25	Course Extender 2	21.2	Kgs
	Course Extender 3	9.5	Kgs
	Course Extender 4	1.4	Kgs
	Wetting Agent	0.045	Kgs
	Pliotite A.C.4*	7.13	Kgs
30	Chlorinated Paraffin 50	4.14	Kgs
	Baggase	10.0	Kgs
	Mineral Spirits	22.77	_
	Polar Solvent	9.54	

BAGASSE: 10 Kgs. This amount represents approx 8.4% by

weight of the total composition.

SILICA: Hollow organo silicon modified borosilicate microspheres: 5 Kgs. This amount represents approx 4.2% by weight of the total composition.

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## Example 7: COPOLYMER HARDEMABLE BASE

#### HARDENABLE BASE:

·	Yellow Iron Oxide	2.9	Kgs
•	Titanium Dioxide	2.9	Kgs
5	Course Extender l	63.0	Kgs
	Course Extender 2	8.6	Kgs
	Wetting Agent	0.6	Kgs
	Pliolite A.C.4*	2.76	Kgs
	Chlorinated Paraffin 70	0.345	Kgs
10	Chlorinated Paraffin 50	2.7	Kgs
	Mineral Spirits	15.0	Kgs
	Polar Solvent	4.3	Kgs

BAGASSE: 15 Kgs. This amount represents approx 12.2% by

weight of the total composition.

15 SILICA: A Hollow organo silicon modified borosilicate

microspheres: 5 Kgs. This amount represents approx 4.1% by weight of the total composition.

## Example 8: COPOLYMER HARDENABLE BASE

#### HARDENABLE BASE:

20	Pliolite A.C.4*	17.25	Kgs
	Non Yellowing	1.75	Kgs
	Plasticizer		
	Mineral Spirits	66.3	Kgs
	Polar Solvent	28.75	Kgs
25	Cleaning Agent	6.46	Kgs
	Aggregate 1.8-2 mm	150-200	gm
	Aggregate 3-4mm	150-200	am

BAGASSE: 15 Kgs. This amount represents 10.7% by weight

of the total composition.

30 SILICA: Hollow organo silican modified borosilicate

microspheres: 5 Kgs.

This amount represents 3.5% by weight of the

total composition.

Example 9: STYRENE ACRYLIC HARDENABLE BASE.

#### HARDENABLE BASE:

	BASF 290D Acrylic*	322	Kgs
	Dispex N40*	3.4	Kgs
5	Beveloid 60*	2.3	Kgs
•	Corflex 880*	4.6	Kgs
	Basf S.300 Acrylic*	32.0	Kgs
	Titanium Dioxide	20.0	Kgs
	Water	52.0	Litres
10	M.D. 13 (Mercury)*	1.75	Kgs
	Corsal EEA*	7.5	Kgs
	White Spirits	11.5	Litres
	Ammonia	2.75	Litres

#### BAGASSE: 195 Kgs.

This amount represents approx 27.1% by weight 15 of the total composition.

Hollow organo silicon modified borosilicate SILICA: microspheres: 65 Kgs. This amount represents approx 9.0% by weight of the total composition.

#### 20 Example 10: ACRYLIC HARDENABLE BASE

#### HARDENABLE BASE:

	Ethylene Glycol	7.41 Kgs
	Water	42.0 Kgs
	Natrasol 250 HR*	.86 Kgs
25	Orotan 731 25%*	2.39 Kgs
	Triton G.F.10*	.20 Kgs
	M.D. 13 (Mercury)*	.5 Kgs
	Texanol*	4.4 Kgs
	Titanium Dioxide	5.0 Kgs
30	Primal AC 388*	115.0 Kgs
	Beveloid 60*	.400 Kgs
	E.T.P	3.0 Kgs
	Water	To Viscosity

BAGASSE: 112 Kgs. This amount represents approx 33.9% by weight of total composition excluding water 45 added for viscosity.

Hollow organo silicon modified borosilicate: SILICA: 37 Kgs. This amount represents approx 11.2% be weight of total composition excluding water added for viscosity.

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## Example 11: ALKYD RESIN BASE

## HARDENABLE BASE:

White Spirits	46	Kgs
Alkyd Resin Ml7	.· <b>92</b>	Kgs
Alkyd Resin M57	92.	Kgs
Cereclor 48*	1	Kgs
Polybutane 100*	6	Kgs
Zinc Oxide	4	Kgs
M.D. 13 (Mercury)*	0.3	Kgs
Crodaclay*	4	Kgs
D.A.A.	1	Litre
	Alkyd Resin M17 Alkyd Resin M57 Cereclor 48* Polybutane 100* Zinc Oxide M.D. 13 (Mercury)* Crodaclay*	Alkyd Resin M17 92 Alkyd Resin M57 92 Cereclor 48* 1 Polybutane 100* 6 Zinc Oxide 4 M.D. 13 (Mercury)* 0.3 Crodaclay* 4

BAGASSE: 153 Kgs. This amount represents approx 34.8%

by weight of the total composition.

SILICA: Hollow organo silican modified borosilicate

microspheres: 40 Kgs. This amount represents approx 9.1% by weight of the total composition.

## Example 12: GELCOAT BASE

#### GELATINOUS HARDENABLE BASE

20		White Spirits Alkyd Resin M57	51 186	Kgs Kgs
		Polybutane 100	6	Kgs
		Zinc Oxide	6	Kgs
		M.D. 13 (Mercury)*	0.3	Kgs
		Crodaclay	2	Kgs
25		D.A.A.	1.5	Kgs
		White Spirits	to vi	scosity
	BAGASSE	190 Kgs. This amount re	eprese	nts approx 39%
		by weight of the total	compos	ition excluding
	•	white spirits added to	viscos	ity.
30	SILICA:	Hollow organo silicon m	odifie	d borosilicate
		microspheres: 45 Kgs.		•
		This amount represents	approx	9.3% by weight

of the total composition.

Example 13: STYRENE ACRYLIC HARDENABLE BASE.

#### HARDENABLE BASE:

BASF 290D Acrylic*	322	Kgs
Dispex N40*	3.4	Kgs
Beveloid 60*	2.3	Kgs
Corflex 880*	4.6	Kgs
Basf S.300 Acrylic*	32.0	Kgs
Titanium Dioxide	60.0	Kgs
Calcium Carbonate		
Water	52.0	Litres
M.D. 13 (Mercury)*	1.75	Kgs
Corsal EEA*	7.5	Kgs
White Spirits	11.5	Litres
Ammonia	2.75	Litres
	Dispex N40* Beveloid 60* Corflex 880* Basf S.300 Acrylic* Titanium Dioxide Calcium Carbonate Water M.D. 13 (Mercury)* Corsal EEA* White Spirits	Dispex N40*  Beveloid 60*  Corflex 880*  Basf S.300 Acrylic*  Titanium Dioxide  Calcium Carbonate  Water  M.D. 13 (Mercury)*  Corsal EEA*  White Spirits  3.4  2.3  4.6  80.0  100.0  100.0  100.0  100.0  100.0  100.0  100.0  100.0

15 <u>SILICA</u>: Hollow organo silicon modified borosilicate microspheres: 80 Kgs. This amount represents approx 11.8% by weight of the total composition.

### Example 14: ACRYLIC HARDENABLE BASE

### HARDENABLE BASE:

20	Ethylene Glycol Water	7.41 42.0	Kgs Kgs
	Natrasol 250 HR*	.86	Kgs
	Orotan 731 25%*	2.39	Kgs
	Triton G.F.10*	.20	Kgs
25	M.D. 13 (Mercury)*	.5	Kgs
	Texanol*	4.4	Kgs
	Titanium Dioxide	15.0	Kgs
	Talc	17.0	Kgs
	Silica 140 Mesh	17.35	Kgs
30	Primal AC 388*	115.0	Kgs
	Silica 140 Mesh	8.67	Kgs
	Beveloid 60*	.400	Kgs
	E.T.P	3.0	Kgs
	Water	To Vi	scosity

35 <u>BAGASSE</u>: 195 Kgs. This amount represents approx 45.4% by weight of total composition excluding water added for viscosity.

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All examples of insulating paints mentioned above (Examples 1 to 14) can be varied and modified to suit particular applications, conditions and purposes. The formulas and compositions may require pigmentation, thereby possibly changing the % by weight of bagasse and silica.

The particular brand of silica (hollow organo silicon modified borosilicate microspheres) utilised is O-CEL\*.

Throughout the specification the appearance of an asterisk (\*) denotes that the substance mentioned is identified by its Trade Mark or registered Trade Mark.

#### PRODUCTION OF INSULATING COATING

when producing a paint or coating in accordance with the present invention the hardenable liquid base mixture is manufactured separately. To this mixture particulated bagasse is added, being of an average particle size of 0.01 mm to 5 mm, and most preferably 0.01 mm to 0.5 mm.

To produce bagasse of the preferred sizes, the raw material is ground or particulated by any means available.

Once the bagasse and the hardenable liquid base have been suitably mixed, the silica is then added. If the silica utilised is hollow organo silicon modified borosilicate microspheres, then it must be the last component added, as the hollow nature of the spheres is such that the sphere can be broken.

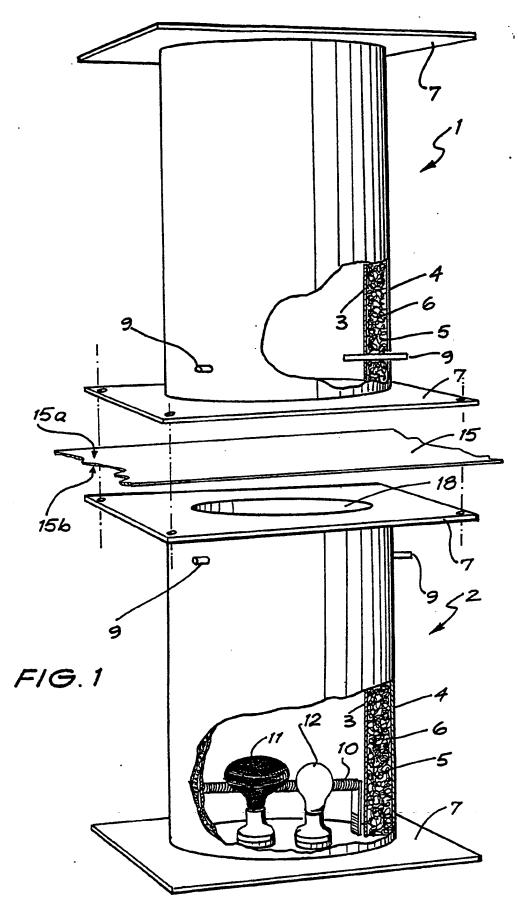
Where an insulation coating is manufactured from a liquid hardenable base and silica alone, then silica can make upto 50% by weight of the total composition.

Where an insulating coating is manufactured from a liquid hardenable base and bagasse alone, then bagasse can make upto 50% by weight of the total composition.

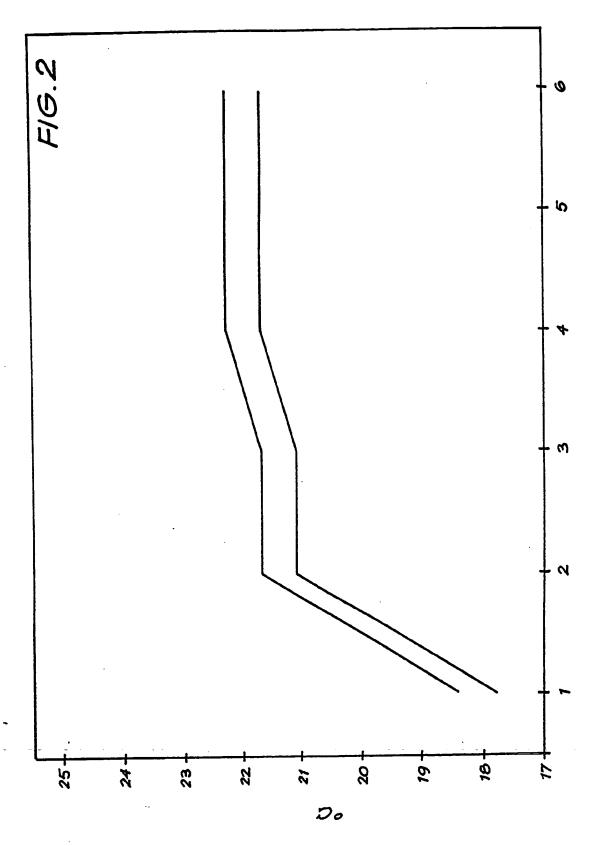
#### THE CLAIMS:

- 1. An insulating coating composition comprising:
- (a) a hardenable liquid base; and
- (b) either silica or bagasse.
- 2. An insulating coating composition as claimed in claim 1, wherein said composition includes both silica and bagasse.
- 3. An insulating coating composition as claimed in claim 1 or 2 wherein the liquid base when hardened forms a high build coating membrane.
- 4. An insulating coating composition as claimed in claims 2 or 3, wherein up to 60% by weight of the coating composition is a combination of silica and bagasse.
- 5. An insulating coating composition as claimed in any one of the preceding claims wherein said bagasse comprises up to 50% by weight of the total composition.
- 6. An insulating coating as claimed in any one of the preceding claims wherein said silica comprises up to 50% by weight of the total composition.
- 7. An insulating coating as claimed in any one of the preceding claims wherein the average particulate size of said bagasse is in the range of 0.01 to 5 mm.
- 8. An insulating coating composition as claimed in any one of the preceding claims, wherein the average particulate size of said bagasse is in the range of 0.01 to 0.5 mm.
- 9. An insulating coating as claimed in any one of the preceding claims wherein said silica is made up any one of the following or a combination of any of the following:
- (a) hollow organo silicon modified borosilicate;
- (b) solid glass microspheres;
- (c) ceramic microspheres;
- (d) polymeric microspheres;
- (e) mineral microspheres.
- 10. An insulating-coating as claimed in any one of the preceding claims wherein when said silica contains hollow organo silicon modified borosilicate microspheres, it is the last component added to the composition.

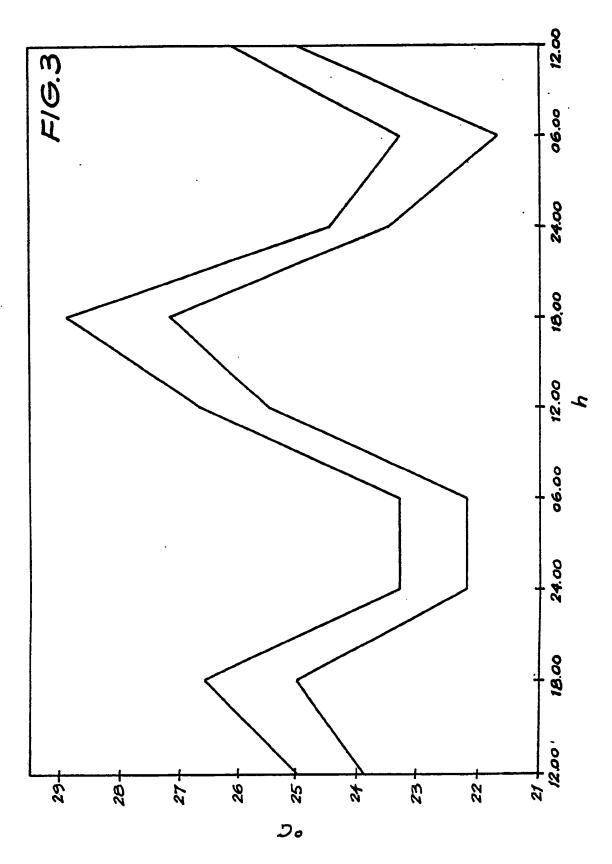
- 11. An insulating coating as claimed in any one of the preceding claims wherein bagasse (the natural substance) is replaced by an artificially produced equivalent.
- 12. A method of producing an insulating coating, said method including the steps of:
- (a) collecting bagasse;
- (t) grinding and/or particulating said bagasse to an average particle size of 0.01 mm to 5 mm; and
- (c) mixing the particulated bagasse into a paint, coating composition or like substance.
- 13. A method of producing an insulating coating as claimed in Claim 12, wherein said bagasse (the natural substance) is replaced by an, artificially produced equivalent.
- 14. An insulating coating being substantially as herein described with reference to the accompanying drawings and examples.
- 15. A method of producing an insulating coating, said method being substantially as herein described with reference to the accompanying drawings and examples.



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## INTERNATIONAL SEARCH REPORT

International Application No PCT/AU 86/00048

		10 80/00046
I. CLASSIF	FICATION OF SUBJECT MATTER (it several classification sympols apply, indicate all) 6	
	International Patent Classification (IPC) or to both National Classification and IPC	
Int.	C1.4 C09D 5/00, 7/12	
II. FIELDS	SEARCHED Minimum Documentation Searched	
<b>O</b> 11011		
Classification	System   Classification Symbols	
IPC	CO9D 5/00, 7/12	
	Documentation Searched other than Minimum Documentation to the Extent that such Documents are included in the Fields Searched <sup>8</sup>	
AU:	IPC as above	
III. DOCUM	MENTS CONSIDERED TO BE RELEVANT	
Category *	Citation of Document, 11 with Indication, where appropriate, of the relevant passages 12	Relevant to Claim No. 13
X	AU, B, 33976/78 (520716) (TORAY INDUSTRIES INC) 13 September 1979 (13.09.79)	(1, 3, 9)
X	DE, A, 2445075 (FUJI KURA CABLE WORKDS L.T.D.) 3 April 1975 (03.04.75)	(1, 3, 9, 10)
X	FR, A, 1466597 (HEIJMER) 20 January 1967 (20.01.67)	(1)
X	US, A, 4277355 (FARCNIK) 7 July 1981 (07.07.81)	(1)
X	JP, A,59058-065 (TORAY INDUSTRIES INC) 3 April 1984 (03.04.84) (Derwent English Language Abstract 84-118595/19)	(1)
А, Р	AU, B, 37653/85 (PPG INDUSTRIES INC) 8 August 1985 (08.08.1985)	
A	US, A, 4351669 (NIELSEN) 28 September 1982 (28.09.82)	
A	US, A, 4240936 (HENNING) 23 December 1980 (23.12.80)	
"A" doct consider con	is categories of cited documents: 19  ument defining the general state of the art which is not sidered to be of particular relevance ier document but published on or after the international g date  ument which may throw doubts on priority claim(s) or ch is cited to establish the publication date of another tion or other special reason (as specified)  ument referring to an oral disclosure, use, exhibition or er means  ument published prior to the international filing date but r than the priority date claimed  "IFICATION  "T" later document published after to or priority date and not in conflicted to understand the priority date and not in conflicted to understand the priority document of particular relevant cannot be considered novel of involve an inventive step  "Quement of particular relevant cannot be considered to involve an inventive step  "Actual Completion of the international Search  "The later document published after to or priority date and not in conflicted to understand the principle invention  "X" document of particular relevant cannot be considered to involve an inventive step  "Actual Completion of the international filing date but to the priority date and not in conflicted to understand the principle invention  "X" document of particular relevant cannot be considered to involve an inventive step  "Actual Completion of the international filing date but to the priority date and not in conflicted to understand the principle invention  "X" document of particular relevant cannot be considered novel of involve an inventive step  "Actual Completion of the international filing date but to the priority date and not in conflicted to understand the principle invention  "X" document priority date and not in conflicted to understand the priority date and not in conflicted to understand the priority decended to another cannot be considered novel of involve an invention of invention and the priority date and not in conflicted to understand the priority decended to another cannot be considered to involve an inve	ict with the application but le or theory underlying the ice; the claimed invention reannet be considered to ice; the claimed invention an inventive step when the or more other such docupations to a person skilled patent family
1	1986 (05.06.86) (13-06-86) 13 Jun	JE 1986
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Remark on Protest

The additional search fees were accompanied by applicant's protest.

No protest accompanied the neumant of additional assets tree.

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# ANNEX TO THE INTERNATIONAL SEARCH REPORT ON INTERNATIONAL APPLICATION NO. PCT/AU 86/00048

This Annex lists the known "A" publication level patent family members relating to the patent documents cited in the above-mentioned international search report. The Australian Patent Office is in no way liable for these particulars which are merely given for the purpose of information.

Patent Document Cited in Search Patent Family Members Report							
AU	33976/78	BR DE JP US	7801476 2810072 53111336 4211823	CA FR NL	1118929 2383220 7802636	CH GB SE	628366 1596107 7802753
DE	2445075	US	50058137 4017155 50061618	CH JP	12061/74 50061433	GB JP	1442249 50051698
US	4277355						<del></del>
AU	37653/85	BR JP	8500396 60181173	EP	153699	ES	539999 .
us	4351669	SE	1149544	СН	645909	DE	3030611
US	4240936	US	4324000	······································		<del></del>	

END OF ANNEX